

## Oxidative Coupling of Methane over a Li<sup>+</sup>/MgO Catalyst Using N<sub>2</sub>O as an Oxidant

HIROSHI YAMAMOTO, HON YUE CHU, MINGTING XU, CHUNLEI SHI,  
AND JACK H. LUNSFORD<sup>1</sup>

*Department of Chemistry, Texas A&M University, College Station, Texas 77843*

Received December 14, 1992; revised February 22, 1993

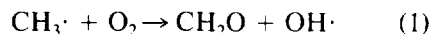
Nitrous oxide is an effective oxidant for the conversion of CH<sub>4</sub> to C<sub>2</sub>H<sub>4</sub> and C<sub>2</sub>H<sub>6</sub> over a Li<sup>+</sup>/MgO catalyst, although the rate of oxygen incorporation into the lattice and the regeneration of the active centers is much slower with N<sub>2</sub>O than with O<sub>2</sub>. Thus, except at very low CH<sub>4</sub> partial pressures, the rate-limiting step is oxygen incorporation, rather than the activation of CH<sub>4</sub> at the surface. Carbon dioxide is a poison for the production of CH<sub>3</sub>· radicals and for the conversion of CH<sub>4</sub>. By extrapolation of the rate data, the rate of CH<sub>4</sub> reaction over the unpoisoned catalyst was determined, and the rate was shown to be first order with respect to N<sub>2</sub>O. A kinetic model, based on competitive surface reactions, in addition to gas-phase reactions, adequately accounts for the conversion as a function of reagent concentrations and temperature, as well as the selectivity for ethane and ethylene. At comparable levels of conversion O<sub>2</sub> is a less selective oxidant than N<sub>2</sub>O, not because of more gas-phase oxidation, but because of surface reactions involving reactive oxygen species. The presence of CH<sub>4</sub> significantly inhibits the decomposition of N<sub>2</sub>O over the catalyst. It is suggested that CH<sub>4</sub> and N<sub>2</sub>O are activated by a common intermediate (e.g., O<sub>2</sub><sup>-</sup> ions) and that CH<sub>4</sub> reacts more rapidly with this species. © 1993 Academic Press, Inc.

### INTRODUCTION

In most studies on the oxidative coupling of CH<sub>4</sub> to C<sub>2</sub>H<sub>6</sub> and C<sub>2</sub>H<sub>4</sub> (C<sub>2</sub> compounds), molecular oxygen has been used as the oxidant. Because the coupling reaction is a complex network of heterogeneous and homogeneous reactions, it is instructive to employ other oxidants, such as nitrous oxide. Otsuka and Nakajima (1) previously obtained kinetic data for the oxidative coupling reaction over Sm<sub>2</sub>O<sub>3</sub>, using N<sub>2</sub>O as the oxidant. They observed that at a relatively low temperature for the oxidative coupling reaction (550°C) N<sub>2</sub>O resulted in the formation of C<sub>2</sub>H<sub>6</sub> with high selectivity, while complete oxidation occurred with O<sub>2</sub> as the oxidant. Moreover, N<sub>2</sub>O decomposition was believed to be the rate-limiting step in the catalytic cycle. Hutchings *et al.* (2, 3) have also compared N<sub>2</sub>O and O<sub>2</sub> as oxidants. They found that over a Li<sup>+</sup>/MgO catalyst the con-

version of CH<sub>4</sub> was an order of magnitude greater with O<sub>2</sub> than with N<sub>2</sub>O when the oxidants were compared at the same pressure, but when the conditions were adjusted such that the conversions were the same, the C<sub>2</sub> selectivities were greater with N<sub>2</sub>O (85% C<sub>2</sub> selectivity with N<sub>2</sub>O and 50% C<sub>2</sub> selectivity with O<sub>2</sub>). Additional results obtained with N<sub>2</sub>O as an oxidant have been reviewed by Hutchings and Scurrall (4).

The origin of CO<sub>2</sub> during the oxidative coupling of CH<sub>4</sub> is still a matter of conjecture; however, it is clear that certain important gas phase reactions occur with O<sub>2</sub>, but not with N<sub>2</sub>O. For example, the reaction



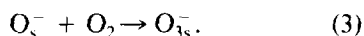
supplies hydroxyl radicals which are known to be chain carriers in the combustion of hydrocarbons. By contrast, the analogous reaction with N<sub>2</sub>O,



does not form OH· radicals. But our previ-

<sup>1</sup> To whom correspondence should be addressed.

ous attempts to model the heterogeneous-homogeneous coupling reaction over  $\text{Li}^+/\text{MgO}$  with  $\text{O}_2$  as the oxidant suggested that gas phase reactions do not account for more than 10% of the  $\text{CO}_x$  at short residence times, at  $700^\circ\text{C}$ , and with low partial pressures of reagents (5). If this is indeed the case, then one must look for other explanations for the differences in selectivities. Molecular oxygen may form a different type of active site on the surface that is responsible for the complete oxidation of the hydrocarbons in the system. Such a site might be  $\text{O}_3^-$  ions, which are known to be formed at low temperatures by the reaction (6)



Here, the subscript "s" refers to a surface species. In stoichiometric reactions ozonide ions were found to be much less selective than  $\text{O}^-$  ions in the dehydrogenation of alkanes over MgO (7).

As an oxidant for a kinetic study  $\text{N}_2\text{O}$  has a distinct advantage over  $\text{O}_2$  with respect to the range of  $\text{CH}_4/\text{O}_2$  ratios that can be explored. At  $\text{CH}_4/\text{O}_2$  ratios  $\leq 1$ , complete combustion begins to dominate, whereas, with  $\text{N}_2\text{O}$  as the oxidant large  $\text{C}_2$  selectivities are observable under differential conditions, even at  $\text{CH}_4/\text{N}_2\text{O}$  ratios of 0.1. As a consequence the entire range of rate-limiting steps may be examined, from oxygen incorporation in the catalyst at one extreme to C-H bond breaking at the other extreme. Since nonselective secondary reactions involving the oxidant are less likely to occur, it also is possible to study the rate of methyl radical formation over a much broader range of oxidant partial pressures with  $\text{N}_2\text{O}$  than with  $\text{O}_2$ . This investigation was carried out in an effort to explore further the mechanism of the oxidative coupling reaction over  $\text{Li}^+/\text{MgO}$  catalysts. It was of particular interest to determine the origin of the apparent activation energies that are obtained under truly rate-limiting conditions.

#### EXPERIMENTAL

The  $\text{Li}^+/\text{MgO}$  catalyst was prepared by heating an aqueous slurry of  $\text{Li}_2\text{CO}_3$  and

MgO (Aldrich) to  $100^\circ\text{C}$  for several hours and then evaporating the water. The dry sample was sieved to 20–45 mesh and calcined in air at  $750^\circ\text{C}$  for 10 h. The amount of lithium loaded on the MgO was 4.1 wt%. After calcination the surface area of the catalyst was  $2.7 \text{ m}^2/\text{g}$ . For comparison, a low-surface-area MgO catalyst was prepared by heating the high purity oxide at  $930^\circ\text{C}$  for 10 h in a sealed fused-quartz tube. The resulting material had a surface area of  $8.5 \text{ m}^2/\text{g}$ . In order to prevent excessive gas pressure, the tube with the catalyst was evacuated at elevated temperatures before sealing.

The kinetic studies were carried out in a plug-flow reactor constructed of fused quartz. The upper section of the reactor, which contained the catalyst, was 10 mm i.d., and the lower section was constructed of 1-mm-i.d. capillary tube. The smaller diameter allowed the products to pass rapidly out of the heated zone. A thermocouple was located at the level of the catalyst on the outside of the reactor. In a separate experiment, the temperature inside the catalyst bed was compared to that measured outside of the reactor, and it was found that the temperature difference was only  $1^\circ\text{C}$ .

All of the kinetic results were obtained under nearly differential conditions. The conversion of the limiting reagent was  $\leq 20\%$ . In these studies 0.731 g (0.79 cc) of  $\text{Li}^+/\text{MgO}$  or 0.269 (0.94 cc) of MgO catalyst was loaded between 1-mm-thick layers of quartz wool. Quartz chips were placed above the catalyst to aid in preheating the reactant gas and to minimize the free volume. A blank experiment was carried out with only quartz chips in the reactor, and it was found that with 40 kPa  $\text{CH}_4$ , 61 kPa  $\text{N}_2\text{O}$ , a flow rate of 50 ml/min, and at  $680^\circ\text{C}$ , the conversion of  $\text{CH}_4$  and  $\text{N}_2\text{O}$  was only 0.1%.

The reactant gases were premixed before entering the reactor using mass flow controllers. The total flow rate was about 50 ml/min. Helium was used as a diluent to achieve a total pressure of 101 kPa. The purities of

the  $\text{CH}_4$  and  $\text{N}_2\text{O}$ , both from Matheson, were 99.97 and 99.0%, respectively. Gas chromatography was used to analyze the product stream. Separation of the various components was achieved using molecular sieve and Porapak R columns.

The rate of  $\text{CH}_4$  consumption generally was calculated from summation of the moles of products, taking into account the stoichiometric factors. At the larger conversion levels the amount of  $\text{CH}_4$  converted also was determined by difference. In such cases the material balance, based on the carbon, was greater than 95%.

Methyl radical formation was obtained using the matrix-isolation electron spin resonance (MI-ESR) system that has been described previously (8). Briefly, radicals which exit a thin layer of catalyst enter a leak into a differentially pumped region. The radicals are frozen in an argon matrix on a sapphire rod maintained at 15 K, and, after a certain collection period, their ESR spectra are recorded. The total pressure in the region of the catalyst was ca. 0.1 kPa.

The kinetic isotope effect (KIE) was obtained from the isotopic distribution of H and D in the ethane product. The experiment was performed using a known mixture of  $\text{CH}_4/\text{CD}_4$ . The sensitivities and fragmentation patterns of pure methanes ( $\text{CH}_4$  and  $\text{CD}_4$ ) and ethane ( $\text{C}_2\text{H}_6$  and  $\text{C}_2\text{D}_6$ ) were first obtained using a GC/MS system at typical experimental conditions, and then the standard fragmentation pattern of  $\text{CH}_3\text{CD}_3$  was calculated. The relative amounts of  $\text{C}_2\text{H}_6$ ,  $\text{CH}_3\text{CD}_3$ , and  $\text{C}_2\text{D}_6$  were calculated based on the mass spectra of the product ethane and the previously determined sensitivities and fragmentation patterns of these three materials. The KIE was then calculated using the relative amount of  $\text{CH}_3$  and  $\text{CD}_3$  in the ethanes. The error associated with the KIE obtained in this manner is estimated to be less than 5%.

## RESULTS

### *Decomposition of $\text{N}_2\text{O}$*

Many metal oxides are known to be effective catalysts for the decomposition of  $\text{N}_2\text{O}$

at elevated temperatures (9, 10); therefore, it was of interest to explore briefly the properties of  $\text{Li}^+/\text{MgO}$  for this reaction. At a pressure of 40 kPa  $\text{N}_2\text{O}$  the conversion of  $\text{N}_2\text{O}$  was studied over the temperature range from 635 to 680°C. The conversion levels were found to be 5 and 15% at 635 to 680°C, respectively. From data obtained over this temperature range an  $E_a$  of  $192 \pm 8$  kJ/mol was determined. Surprisingly, the addition of even 10 kPa  $\text{CH}_4$  had a strong negative effect on the rate of  $\text{N}_2\text{O}$  reaction over the  $\text{Li}^+/\text{MgO}$  catalyst. Based on the amount of  $\text{N}_2$  that appeared in the gas phase, the  $\text{N}_2\text{O}$  decomposition decreased to 1 and 2.5% at 635 and 680°C, respectively. When the  $\text{CH}_4$  pressure was increased to 30 kPa, the effect on the  $\text{N}_2\text{O}$  reaction was essentially the same. As will be subsequently shown, the amount of  $\text{O}_2$  in the gas phase was very small when  $\text{CH}_4$  was present. The negative effect of  $\text{CH}_4$  on the catalytic decomposition of  $\text{N}_2\text{O}$  is an advantage for this study, as the presence of relatively large amounts of  $\text{O}_2$  would complicate the interpretation of the following results.

### *Kinetic Data for Oxidative Coupling*

Conversion and selectivity data were obtained for the reaction of  $\text{CH}_4$  with  $\text{N}_2\text{O}$  over the temperature range from 635 to 680°C. Selected data, obtained by varying the partial pressure of  $\text{CH}_4$  from 5 kPa to 40 kPa, while keeping the partial pressure of  $\text{N}_2\text{O}$  constant at about 60 kPa, are shown in Table I and Fig. 1. As noted in Table I, the  $\text{C}_{2+}$  selectivity was quite large (70 to 91%) even though the methane-to-oxidant ratio was considerably less than unity. With  $\text{O}_2$  as the oxidant, even at a  $\text{CH}_4/\text{O}_2$  ratio of 5.4 (see below), the  $\text{C}_{2+}$  selectivity was only 62% for 10.7%  $\text{CH}_4$  conversion at 680°C. Because of the larger selectivity obtained with  $\text{N}_2\text{O}$  the absolute amount of  $\text{CO}_2$  produced was small and the poisoning effect of  $\text{CO}_2$  was less severe. The amount of  $\text{O}_2$  that appeared as a product was negligible, therefore its role in the oxidation process (both heterogeneously and homogeneously) can be largely

TABLE I  
Effect of CH<sub>4</sub> Partial Pressure on the Catalytic Reaction over Li<sup>+</sup>/MgO

CH <sub>4</sub> /N <sub>2</sub> O <sup>a</sup> (kPa)	CH <sub>4</sub> Conv. (%)	Selectivity (%)				CO <sub>2</sub> <sup>b</sup> (kPa)	O <sub>2</sub> <sup>c</sup> (kPa)
		C=C	C-C	C <sub>3</sub>	CO <sub>2</sub>		
4.3/59.4	21.2(21.3) <sup>d</sup>	40(15)	22(52)	7(0.6)	30(24)	0.28	0.01
8.9/60.1	14.2(14.9)	39(14)	29(60)	9(0.6)	22(19)	0.27	0.01
19.1/60.4	8.6(8.3)	37(11)	38(66)	11(0.5)	13(15)	0.22	0.00
38.1/59.6	4.7(4.3)	32(9)	49(69)	10(0.3)	9(14)	0.16	0.00

<sup>a</sup> Pressure of reactants,  $T = 680^\circ\text{C}$ .

<sup>b</sup> The CO<sub>2</sub> in the system was derived from the reaction.

<sup>c</sup> The O<sub>2</sub> in the system was derived from the reaction.

<sup>d</sup> The numbers in parentheses were determined from the model (see text).

discounted. Similarly, the amount of CO formed was below the detection limits.

The rate of CH<sub>4</sub> conversion, as shown in Fig. 1, increased with increasing partial pressure of CH<sub>4</sub> up to about 10 kPa, but at higher partial pressures the reaction became almost zero order with respect to CH<sub>4</sub> pressure. The effect of CO<sub>2</sub> produced during the reaction will be subsequently discussed; however, at this point it is sufficient to note from the data of Table 1 that at 680°C the amount of CO<sub>2</sub> decreased from 0.28 to 0.16 kPa as the CH<sub>4</sub> partial pressure was increased from 4.3 to 38.1 kPa. At a constant

level of CO<sub>2</sub> poisoning the conversion, for example at 4.3 kPa in Fig. 1, would be increased about 30%. The net result is that after factoring out the effect of varying CO<sub>2</sub> partial pressures the reaction would become zero order with respect to CH<sub>4</sub> at even lower partial pressures than indicated in Fig. 1.

The results obtained while keeping the partial pressure of CH<sub>4</sub> constant at ca. 9.5 kPa and varying the pressure of N<sub>2</sub>O are summarized in Table 2 and Fig. 2. Again, the selectivity for C<sub>2+</sub> products was large ( $\geq 80\%$ ), and almost no O<sub>2</sub> was formed. From Fig. 2 it appears that the orders with respect to CH<sub>4</sub> and N<sub>2</sub>O are similar; however, the consequences of CO<sub>2</sub> poisoning

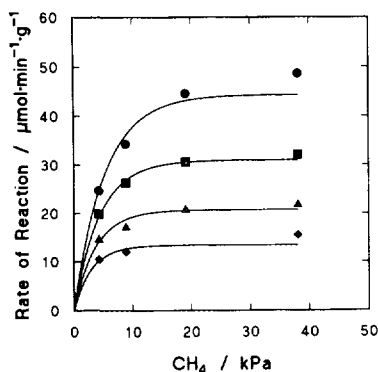


FIG. 1. Dependence of CH<sub>4</sub> consumption over Li<sup>+</sup>/MgO on CH<sub>4</sub> pressure, while keeping the N<sub>2</sub>O pressure constant at ca. 60 kPa: (◆) 635°C, (▲) 650°C, (■) 665°C, and (●) 680°C. The solid lines were calculated using the model.

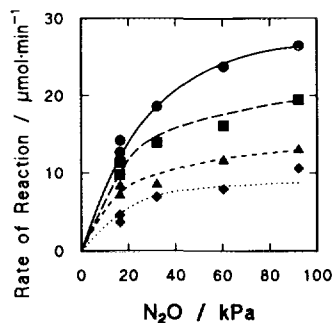


FIG. 2. Dependence of CH<sub>4</sub> consumption over Li<sup>+</sup>/MgO on N<sub>2</sub>O pressure, while keeping the CH<sub>4</sub> pressure constant at ca. 10 kPa: (◆) 635°C, (▲) 650°C, (■) 665°C, and (●) 680°C.

TABLE 2

Effect of N<sub>2</sub>O Partial Pressure on the Catalytic Reaction over Li<sup>+</sup>/MgO

CH <sub>4</sub> /N <sub>2</sub> O <sup>a</sup> (kPa)	CH <sub>4</sub> Conv. (%)	Selectivity (%)					CO <sub>2</sub> <sup>b</sup> (kPa)	O <sub>2</sub> <sup>c</sup> (kPa)
		C=C	C-C	C <sub>3</sub>	CO <sub>2</sub>	CO		
9.6/16.4	4.9	32	52	6	9	0	0.04	0.01
9.8/16.5	5.4	32	51	8	9	0	0.05	
9.2/32.1	7.5	36	44	9	12	0	0.08	0.01
8.7/60.4	10.4	36	37	11	16	0	0.15	0.02
9.2/92.2	10.7	36	35	9	20	0	0.20	0.03

<sup>a</sup> Pressure of reactants, *T* = 680°C.<sup>b</sup> The CO<sub>2</sub> in the system was derived from the reaction.<sup>c</sup> The O<sub>2</sub> in the system was derived from the reaction.

are very different for the two cases. Although the *total* pressure of CO<sub>2</sub> remained small, a fivefold increase in CO<sub>2</sub> pressure occurred as the N<sub>2</sub>O pressure was increased from 16.4 kPa to 92.2 kPa. This means that the intrinsic (i.e., unpoisoned) rates of reaction may be significantly greater than those shown in Fig. 2, particularly at the greater N<sub>2</sub>O pressures.

To determine quantitatively the effect of CO<sub>2</sub> poisoning a series of experiments was carried out in which CO<sub>2</sub> was added to the gas stream. One set of results is shown in Fig. 3, where it is evident that even small partial pressures of CO<sub>2</sub> have a remarkable poisoning effect. In this figure the pressure of CO<sub>2</sub> corresponds to that produced during

the reaction plus any that was added to the reagents. The points at the lowest CO<sub>2</sub> level were obtained without the addition of any CO<sub>2</sub>.

Obviously one would like to know the intrinsic activity of the unpoisoned catalyst in order to obtain the true order of reaction with respect to N<sub>2</sub>O. In a previous kinetic study, with O<sub>2</sub> as the oxidant, Ross and co-workers (11) factored out the effect of CO<sub>2</sub> by adding a rather large amount of CO<sub>2</sub> to the system, thus the reaction became pseudo zero order with respect to CO<sub>2</sub>. We have chosen to extrapolate the rate data to zero CO<sub>2</sub> pressure, using the rate equation

$$R = \frac{k \cdot f[P(\text{CH}_4) \cdot P(\text{N}_2\text{O})]}{1 + K \cdot P(\text{CO}_2)} \quad (4)$$

This is the classic equation that one would obtain for a Rideal mechanism in which one of the products is a poison (12). At constant CH<sub>4</sub> and N<sub>2</sub>O pressures the inverse of Eq. (4) yields

$$\frac{1}{R} = A + B \cdot P(\text{CO}_2) \quad (5)$$

Indeed, a plot of 1/*R* versus CO<sub>2</sub> pressure yields a linear relationship (Fig. 4) and from the ordinate intercept the unpoisoned rate can be determined. The rate of reaction is equated to the rate of C<sub>2+</sub> formation in order to avoid the errors that would be introduced

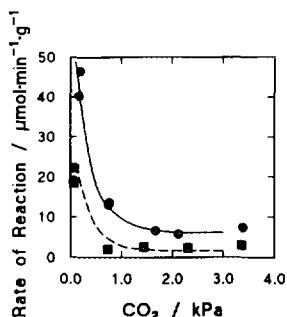


FIG. 3. The effect of CO<sub>2</sub> on the rate of CH<sub>4</sub> conversion to C<sub>2+</sub> products over Li<sup>+</sup>/MgO: *P*(CH<sub>4</sub>) = 30 kPa, *P*(N<sub>2</sub>O) = 70 kPa: (■) 650°C and (●) 680°C.

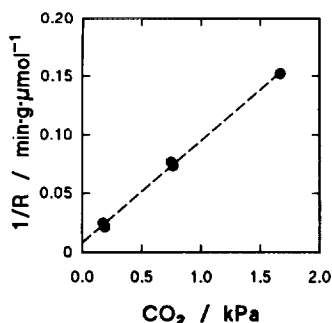


FIG. 4. Inverse rate of  $\text{CH}_4$  conversion to  $\text{C}_2+$  products as a function of  $\text{CO}_2$  partial pressure:  $P(\text{CH}_4) = 30$  kPa,  $P(\text{N}_2\text{O}) = 70$  kPa;  $T = 680^\circ\text{C}$ .

by determining the small amount of  $\text{CO}_2$  that was formed during reaction in the presence of a large amount of added  $\text{CO}_2$ . The error introduced by equating the rates is small as the  $\text{C}_2+$  selectivity was large.

The poisoning experiments were carried out under four sets of conditions, and the results are shown in Fig. 5. Based on the

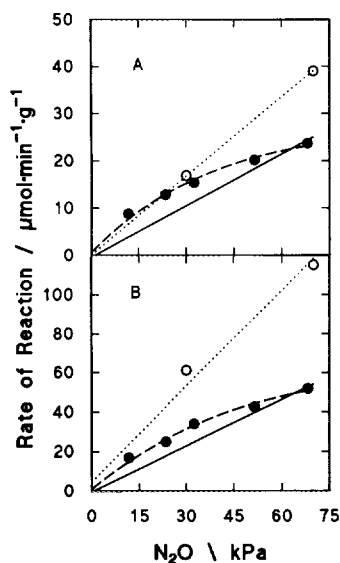


FIG. 5. Comparison of uncorrected (●) and corrected (○) rates for the conversion of  $\text{CH}_4$  as a function of  $\text{N}_2\text{O}$  pressure. The corrected values were obtained by extrapolation of the rates to zero partial pressure of  $\text{CO}_2$  at (A)  $650^\circ\text{C}$  and (B)  $680^\circ\text{C}$ . The solid lines were calculated using the model.

TABLE 3

KIE Results for Methane Oxidation over  $\text{Li}^+/\text{MgO}$ 

Methane <sup>a</sup> (kPa)	KIE	
	Measured	Calculated <sup>b</sup>
2	1.6	1.5
20	1.1	1.1

<sup>a</sup>  $P(\text{N}_2\text{O}) = 60$  kPa,  $T = 680^\circ\text{C}$ .

<sup>b</sup> Determined from the model (see text).

corrected rates it appears that the reaction is first order with respect to  $\text{N}_2\text{O}$ . The zero-order behavior with respect to  $\text{CH}_4$  and first-order behavior with respect to  $\text{N}_2\text{O}$  suggest that oxygen incorporation into the lattice is the rate-limiting step in the mechanism. This is supported by a measure KIE near unity for the oxidation of methane with  $\text{N}_2\text{O}$  at  $700^\circ\text{C}$  (13). The KIEs were determined for  $\text{CH}_4$ -to- $\text{N}_2\text{O}$  ratios of 1:3 and 1:8 at a total pressure of 760 Torr (no diluent). The range of the KIE measurements has been extended to more closely match the conditions of this experiment, and the results are shown in Table 3. Clearly, if the  $\text{CH}_4$  pressure is sufficiently reduced ( $<2$  kPa), the breaking of the C-H bond becomes rate limiting.

From the results of Figs. 1 and 2 the activation energies reported in Table 4 were

TABLE 4

Activation Energy for  $\text{CH}_4$  Oxidation over  $\text{Li}^+/\text{MgO}$ 

$\text{CH}_4/\text{N}_2\text{O}$ (kPa)	$E_a$ (kJ/mol)	$\text{CO}_2^a$ (kPa)
9.2/32.1	$170.8 \pm 6.7$	0.02–0.08
8.7/60.4	$175.0 \pm 4.2$	0.04–0.15
9.2/92.2	$158.2 \pm 10.8$	0.05–0.20
4.3/59.4	$139.0 \pm 7.5$	0.08–0.28
8.9/60.1	$157.4 \pm 5.0$	0.07–0.27
19.1/60.4	$182.9 \pm 2.5$	0.08–0.22
38.1/59.6	$187.9 \pm 9.6$	0.05–0.16

<sup>a</sup> The  $\text{CO}_2$  in the system was derived from the reaction.

TABLE 5

Comparison of O<sub>2</sub> and N<sub>2</sub>O as Oxidants for the Oxidative Coupling of CH<sub>4</sub>

Oxidant	Temp. (°C)	CH <sub>4</sub> Conv. <sup>a</sup> (%)	Selectivity (%)					CO <sub>2</sub> <sup>b</sup> (kPa)	O <sub>2</sub> <sup>c</sup> (kPa)
			C=C	C-C	C <sub>3</sub>	CO <sub>2</sub>	CO		
O <sub>2</sub>	635	3.0	7	22	1	46	25	0.42	4.62
O <sub>2</sub>	646	3.9	10	24	1	44	21	0.53	4.36
O <sub>2</sub>	665	7.1	16	37	2	34	11	0.76	3.76
O <sub>2</sub>	680	10.7	22	36	4	32	6	1.06	3.07
N <sub>2</sub> O	635	2.2	16	63	12	9	0	0.05	0.01
N <sub>2</sub> O	650	3.1	23	59	10	9	0	0.08	0.01
N <sub>2</sub> O	665	4.8	29	50	11	9	0	0.12	0.01
N <sub>2</sub> O	680	6.8	35	44	11	10	0	0.19	0.01

<sup>a</sup> Reaction conditions:  $P(\text{CH}_4) = 30$  kPa,  $P(\text{O}_2) = 5.6$  kPa, and  $P(\text{N}_2\text{O}) = 68$  kPa.<sup>b</sup> The CO<sub>2</sub> in the system was derived from the reaction.<sup>c</sup> The O<sub>2</sub> remaining in the system after being consumed by reaction.

determined. Over the range for which oxygen incorporation was rate limiting, the  $E_a$  was approximately  $167 \pm 8$  kJ/mol; only at the lowest CH<sub>4</sub> partial pressure did the  $E_a$  decrease to  $138 \pm 8$  kJ/mol. One should keep in mind that CO<sub>2</sub> poisoning also has an effect on  $E_a$ , although the effect may be different on the steeper part of the CO<sub>2</sub> adsorption isotherm (see Fig. 3), which is the case with N<sub>2</sub>O, than on the flatter part of the isotherm, which is applicable with O<sub>2</sub>.

#### Comparison of N<sub>2</sub>O and O<sub>2</sub> as Oxidants

In this study an attempt was made to compare N<sub>2</sub>O and O<sub>2</sub> as oxidants at a nearly equal level of CH<sub>4</sub> conversion. This was achieved by measuring the CH<sub>4</sub> conversion level at an arbitrary set of N<sub>2</sub>O and CH<sub>4</sub> pressures, and then substituting O<sub>2</sub> for N<sub>2</sub>O. The O<sub>2</sub> pressure was adjusted such that the CH<sub>4</sub> conversions were similar at 646–650°C. The results, as shown in Table 5, may be summarized as follows: (i) comparable CH<sub>4</sub> conversions were achieved at a much lower partial pressure of O<sub>2</sub>, (ii) the C<sub>2+</sub> selectivity was greater with N<sub>2</sub>O as the oxidant, (iii) a considerable amount of C<sub>3</sub> product was found with N<sub>2</sub>O, and (iv) CO was detected only in the presence of O<sub>2</sub>.

#### Comparison of Li<sup>+</sup>/MgO and MgO as Catalysts

It has previously been reported that with O<sub>2</sub> as an oxidant pure MgO is a rather poor

catalyst for the coupling reaction, both with respect to activity and selectivity (14). From the results of Table 6, it is evident that with N<sub>2</sub>O as the oxidant MgO is also a nonselective catalyst, but the conversion was actually greater over the MgO. This implies that the poor selectivity of MgO is an intrinsic property of the material and is not related to the oxidant. With respect to the activity, one should note that the surface area of MgO was about three times that of the Li<sup>+</sup>/MgO catalyst, therefore the specific activity of MgO is somewhat less than that of the Li<sup>+</sup>/MgO catalyst.

#### MIESR Results

Methyl radical formation was observed over the Li<sup>+</sup>/MgO catalyst both at small and large CH<sub>4</sub>/N<sub>2</sub>O ratios. The Arrhenius plots, shown in Fig. 6, reveal that the rate of production of CH<sub>3</sub>· radicals increases with N<sub>2</sub>O partial pressure. Previously it was reported that the CH<sub>3</sub>· radical production rate increased almost linearly with respect to N<sub>2</sub>O pressure up to a CH<sub>4</sub>/N<sub>2</sub>O ratio of unity, and at larger N<sub>2</sub>O pressures the rate did not increase substantially (13). At a CH<sub>4</sub>/N<sub>2</sub>O ratio of 0.29, a KIE of  $1.9 \pm 0.2$  was observed, whereas at a CH<sub>4</sub>/N<sub>2</sub>O ratio of 44, a KIE of  $1.2 \pm 0.2$  was determined. These results are consistent with a change in the rate limiting step from C–H bond breaking to

TABLE 6  
Comparison of Performance of Li<sup>+</sup>/MgO and MgO Catalysts

Catalyst	CH <sub>4</sub> conv. <sup>a</sup> (%)	Selectivity (%)					CO <sub>2</sub> <sup>c</sup> (kPa)	O <sub>2</sub> <sup>d</sup> (kPa)
		C=C	C-C	C <sub>3</sub>	CO <sub>2</sub>	CO		
MgO <sup>a</sup>	4.6	5	9	1	76	10	1.01	0.08
Li/MgO <sup>b</sup>	2.6	20	60	11	8	0	0.06	0.01

<sup>a</sup> Reaction conditions:  $P(\text{CH}_4) = 29 \text{ kPa}$ ,  $P(\text{N}_2\text{O}) = 50 \text{ kPa}$ ;  $T = 650^\circ\text{C}$ .

<sup>b</sup> Surface area =  $8.5 \text{ m}^2/\text{g}$ .

<sup>c</sup> Surface area =  $2.7 \text{ m}^2/\text{g}$ .

<sup>d</sup> The CO<sub>2</sub> in the system was derived from the reaction.

<sup>e</sup> The O<sub>2</sub> in the system was derived from the reaction.

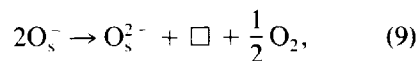
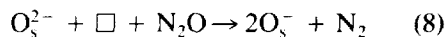
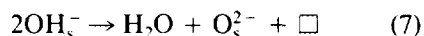
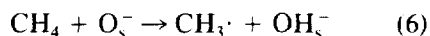
oxygen incorporation as the CH<sub>4</sub>/N<sub>2</sub>O ratio increased. The change in  $E_a$  at  $700^\circ\text{C}$  from  $75 \pm 16$  to  $134 \pm 8 \text{ kJ/mol}$  as the CH<sub>4</sub>/N<sub>2</sub>O ratio increased also is consistent with the change in the rate-limiting step. Apparently, when the temperature becomes  $<600^\circ\text{C}$ , the rate-limiting step changes at the large CH<sub>4</sub>/N<sub>2</sub>O ratios, and it becomes the same as at the small CH<sub>4</sub>/N<sub>2</sub>O ratios; namely, C-H bond breaking. The  $E_a$  associated with this rate-limiting step is  $134 \pm 8 \text{ kJ/mol}$ . It is important to note that these  $E_a$  values were obtained under catalytic conditions, but at very low CO<sub>2</sub> partial pressures. As pointed

out previously, the rate limiting step may be a function of the total pressure, as well as the CH<sub>4</sub>/N<sub>2</sub>O ratio and the temperature.

When CO<sub>2</sub> was substituted for Ar as the matrix-forming gas, there was a dramatic decrease in the production of CH<sub>3</sub>· radicals, and the  $E_a$  increased by about  $84 \text{ kJ/mol}$ . A similar phenomenon was observed with O<sub>2</sub> as the oxidant (15). It follows from Eq. (4) that if  $K \cdot P(\text{CO}_2) \gg 1$ ,  $E_a = E + \lambda$ , where  $\lambda$  is the heat of adsorption (or reaction) of CO<sub>2</sub>. From the results of Fig. 6, one may conclude that  $\lambda = 84 \text{ kJ/mol}$ , as was previously deduced with O<sub>2</sub> as the oxidant.

#### DISCUSSION

The mechanism first proposed by Ito *et al.* (16) for the oxidative coupling of CH<sub>4</sub> over Li<sup>+</sup>/MgO catalysts may be modified to include N<sub>2</sub>O as the oxidant,



where  $\square$  is an oxide ion vacancy. An analogous set of reactions could be written with O<sub>2</sub><sup>2-</sup> ions as the centers responsible for the activation of CH<sub>4</sub>. If one assumes that reaction (8) is rate limiting, then the rate law

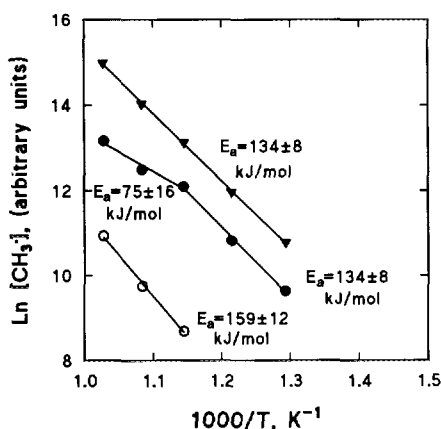


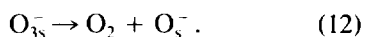
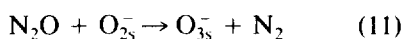
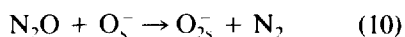
Fig. 6. Arrhenius plots for CH<sub>3</sub>· radical formation: (▼) CH<sub>4</sub>/N<sub>2</sub>O = 1.1/3.8 ml min<sup>-1</sup>, (●) Ar/CH<sub>4</sub>/N<sub>2</sub>O = 3.8/1.1/0/0.25 ml min<sup>-1</sup>, and (○) CO<sub>2</sub>/CH<sub>4</sub>/N<sub>2</sub>O = 3.8/1.1/0/0.25 ml min<sup>-1</sup> at STP.



would be first order with respect to N<sub>2</sub>O and zero order with respect to CH<sub>4</sub>, as was observed over most of the range of conditions in the conventional catalytic experiments. In such a case the apparent activation energy of 75 ± 17 kJ/mol for CH<sub>3</sub>· radical formation might be equivalent to the true activation energy for reaction (8). However, N<sub>2</sub>O and CH<sub>4</sub> also may compete for the same active center, (see below) which would result in a more complex relationship for E<sub>a</sub>. This phenomenon may explain the difference between E<sub>a</sub> values of 167 ± 8 and 75 ± 17 kJ/mol obtained in the conventional mode and in the MIESR system, with both being carried out under conditions at which reaction (8) is rate limiting. Carbon dioxide poisoning also may contribute to this difference.

It is tempting to equate the E<sub>a</sub>'s of 138 ± 8 and 134 ± 8 kJ/mol obtained in the conventional reactor and the MIESR system, respectively, under conditions such that C–H bond breaking was rate limiting. The E<sub>a</sub> obtained in the conventional reactor may have been subject to small effects of CO<sub>2</sub> poisoning. Nevertheless, assuming that such a comparison can be made, the value of 134 kJ/mol is not the activation energy for the C–H bond breaking step alone, but rather it is a linear combination of energies for several steps in the catalytic cycle.

In order to understand the negative effect of CH<sub>4</sub> on N<sub>2</sub>O decomposition additional reactions should be included in the mechanism, for example, by adding the reactions

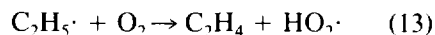


Here it becomes evident that CH<sub>4</sub> and N<sub>2</sub>O may compete for the same O<sub>s</sub><sup>-</sup> center via reactions (6) and (10). Thus, the presence of CH<sub>4</sub> would decrease the rate of N<sub>2</sub>O decomposition. Apparently the rate of reaction (6) is considerably greater than that of reaction (10), as indicated by the strong neg-

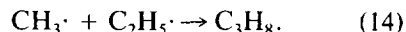
ative effect of CH<sub>4</sub> on N<sub>2</sub>O decomposition. As a consequence very little O<sub>2</sub> is produced via reaction (12), and also the overall consumption of CH<sub>4</sub> is first order, not zero or negative order with respect to N<sub>2</sub>O. Unlike CO<sub>2</sub>, N<sub>2</sub>O serves both to produce and to remove active centers.

There is no direct evidence for reaction 10; however, reaction (11) was previously studied on MgO, and it was found to occur at T ≥ 100°C (17). Reaction (12) was also demonstrated when N<sub>2</sub>O, and presumably a small amount of O<sub>2</sub>, were removed at 25°C from a MgO sample that had O<sub>3s</sub><sup>-</sup> ions (17). The mechanism for N<sub>2</sub>O decomposition via reactions (8)–(12) avoids the problem of electron transfer from an insulator or p-type oxide to N<sub>2</sub>O that is inherent in the mechanisms of Dell *et al.* (9) and Winter (10).

The kinetic model that was previously developed to study the heterogeneous-homogeneous reactions during oxidative coupling with O<sub>2</sub> as the oxidant (13) has been extended to include N<sub>2</sub>O. The original 156 gas-phase reactions were included, as well as the additional reactions shown in Table 7. The reactions of N<sub>2</sub>O with several important intermediates were included, in addition to reactions involving C<sub>3</sub> molecules. Qualitatively, the enhanced formation of C<sub>3</sub> products can be attributed to the competitive reactions



and



If molecular oxygen is present, reaction (13) is an efficient means of converting ethyl radicals to ethylene, but in its absence reaction (14) becomes competitive with the unimolecular decomposition of ethyl radicals.

In the model the rate constants for the heterogeneous reactions (6)–(9) were treated as adjustable parameters, and reactions (10)–(12) were not included. The calculated results using  $k_6 = 2.53 \times 10^{-15} e^{-500/T} \text{ cm}^3 \cdot \text{molecule}^{-1} \cdot \text{s}^{-1}$ ,  $k_7 = 2.00 \times 10^{-5} e^{-0/T} \text{ cm}^3 \cdot \text{molecule}^{-1} \cdot \text{s}^{-1}$ ,  $k_8 = 4.42 \times$

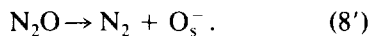
TABLE 7

Gas-Phase Reactions in the Heterogeneous-Homogeneous Model Rate constants

 $k = AT^n \exp[-E_a/RT]$ , in units of  $\text{mol} \cdot \text{cm}^{-3} \cdot \text{s}^{-1}$ 

Reaction	$\log(A)$	$n$	$E_a/R$	Reference
$\text{H} + \text{N}_2\text{O} = \text{NH} + \text{NO}$	14.80	0	14594	(18)
$\text{H} + \text{N}_2\text{O} = \text{OH} + \text{N}_2$	13.88	0	7599	(18)
$\text{O} + \text{N}_2\text{O} = \text{NO} + \text{NO}$	13.65	0	12128	(18)
$\text{O} + \text{N}_2\text{O} = \text{N}_2 + \text{O}_2$	13.65	0	12128	(18)
$\text{OH} + \text{N}_2\text{O} = \text{HO}_2 + \text{N}_2$	8.38	0	0	(18)
$\text{CH}_3 + \text{N}_2\text{O} = \text{CH}_3\text{O} + \text{N}_2$	14.72	0	14276	(18)
$\text{CH}_4 + \text{C}_3\text{H}_5 = \text{CH}_3 + \text{C}_3\text{H}_6$	11.69	0	11258	(18)
$\text{CH}_4 + n\text{-C}_3\text{H}_7 = \text{CH}_3 + \text{C}_3\text{H}_8$	-1.62	4.02	5470	(19)
$\text{CH}_4 + i\text{-C}_3\text{H}_7 = \text{CH}_3 + \text{C}_3\text{H}_8$	-3.14	4.40	5440	(19)
$\text{CH}_3 + \text{C}_2\text{H}_4 = n\text{-C}_3\text{H}_7$	11.52	0	3877	(18)
$\text{CH}_3 + \text{C}_2\text{H}_5 = \text{C}_3\text{H}_8$	14.69	-0.5	0	(18)
$\text{CH}_3 + \text{C}_2\text{H}_2 = \text{C}_3\text{H}_5$	11.78	0	3877	(18)
$\text{CH}_3 + \text{C}_2\text{H}_3 = \text{C}_3\text{H}_6$	13.00	0	0	(20)
$\text{CH}_3 + \text{C}_3\text{H}_8 = \text{CH}_4 + n\text{-C}_3\text{H}_7$	12.34	0	6054	(18)
$\text{CH}_3 + \text{C}_3\text{H}_8 = \text{CH}_4 + i\text{-C}_3\text{H}_7$	12.08	0	5183	(18)
$\text{CH}_3 + \text{C}_3\text{H}_6 = \text{CH}_4 + \text{C}_3\text{H}_5$	10.64	0	3789	(18)
$n\text{-C}_3\text{H}_7 + \text{O}_2 = \text{HO}_2 + \text{C}_3\text{H}_6$	12.00	0	2530	(21)
$i\text{-C}_3\text{H}_7 + \text{O}_2 = \text{HO}_2 + \text{C}_3\text{H}_6$	12.00	0	1503	(21)
$n\text{-C}_3\text{H}_7 = \text{CH}_3 + \text{C}_2\text{H}_4$	38.27	0	16718	(18)
$n\text{-C}_3\text{H}_7 = \text{C}_3\text{H}_6 + \text{H}$	37.78	0	18763	(18)
$i\text{-C}_3\text{H}_7 = \text{CH}_3 + \text{C}_2\text{H}_4$	35.78	0	20567	(18)
$i\text{-C}_3\text{H}_7 = \text{C}_3\text{H}_6 + \text{H}$	38.08	0	19485	(18)
$n\text{-C}_3\text{H}_7 + \text{H}_2 = \text{H} + \text{C}_3\text{H}_8$	12.42	0	7448	(18)
$i\text{-C}_3\text{H}_7 + \text{H}_2 = \text{H} + \text{C}_3\text{H}_8$	12.40	0	8047	(22)
$n\text{-C}_3\text{H}_7 + \text{H} = \text{CH}_3 + \text{C}_2\text{H}_5$	13.03	0	0	(18)
$n\text{-C}_3\text{H}_7 + \text{H} = \text{C}_3\text{H}_8$	13.40	0	0	(19)
$i\text{-C}_3\text{H}_7 + \text{H} = \text{C}_3\text{H}_8$	13.30	0	0	(21)
$\text{C}_3\text{H}_6 + \text{OH} = \text{CH}_2\text{O} + \text{C}_2\text{H}_5$	12.90	0	0	(23)
$\text{C}_3\text{H}_6 + \text{OH} = \text{H}_2\text{O} + \text{C}_3\text{H}_5$	12.88	0	0	(18)
$\text{C}_3\text{H}_6 + \text{H} = \text{H}_2 + \text{C}_3\text{H}_5$	11.81	0	2237	(18)
$\text{C}_3\text{H}_5 + \text{H} = \text{C}_3\text{H}_6$	13.30	0	0	(24)

$10^9 e^{-23,600/T} \text{ s}^{-1}$ , and  $k_9 = 4.82 \times 10^{-13} e^{-0/T}$  are shown in Figs. 1 and 5, and the selectivities are given in Table 1. For computational purposes, reaction (8) was replaced by



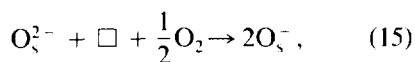
The activation energies for  $k_6$  and  $k_8$  were 4.1 and 196.2 kJ/mol, respectively. By suitably adjusting the preexponential factor an equally good fit to the data of Fig. 1 could be achieved upon increasing the  $E_a$  for  $k_6$  to 40 kJ/mol; however, the fit was not nearly as good in the region of low  $\text{CH}_4$  pressure

when  $E_a$ 's of 80 or 120 kJ/mol were used in the model. The model accurately predicts the functional relationships between the rate of  $\text{CH}_4$  conversion and the partial pressures of  $\text{CH}_4$  or  $\text{N}_2\text{O}$ , as well as the temperature effects. No assumptions are necessary concerning the rate-limiting step. The set of rate constants used to fit the data probably are not unique. The extrapolated rates in Fig. 5 were greater than the calculated rates because the model did not include  $\text{CO}_2$  poisoning effects. When all gas-phase reactions were deleted from the model except the coupling of  $\text{CH}_3\cdot$  radicals, the  $\text{CH}_4$  conversion at 680°C, 8.9 kPa  $\text{CH}_4$  and 60 kPa  $\text{N}_2\text{O}$  de-

creased from 15.0 to 11.9%. Thus, radical reactions in the gas phase result in only 3% more CH<sub>4</sub> conversion. The model also accurately predicts the change in the rate-limiting step as indicated by the KIEs (Table 3).

As shown in Table 1, the calculated selectivities for the combined C<sub>2</sub> products and CO<sub>2</sub> were in good agreement with those found experimentally. This agreement is surprising as the model did not include secondary reactions between the intermediates or stable products and the catalyst. We conclude, therefore, that CO<sub>2</sub> is formed primarily from the oxidation of C<sub>2</sub>'s in the gas phase, in contrast to the case with O<sub>2</sub> as the oxidant at these temperatures. Here it should be noted that the model does include the heterogeneous conversion of CO to CO<sub>2</sub>. In contrast to the agreement in overall C<sub>2</sub> selectivity, it is evident that the model predicts a much smaller C<sub>2</sub>H<sub>4</sub>/C<sub>2</sub>H<sub>6</sub> ratio than was observed experimentally, which confirms that the oxidative dehydrogenation of C<sub>2</sub>H<sub>6</sub> occurs catalytically. The model similarly underestimates the formation of C<sub>3</sub> products, which involves the same C<sub>2</sub>H<sub>5</sub>· radicals (reaction (14)) as in the conversion of C<sub>2</sub>H<sub>6</sub> to C<sub>2</sub>H<sub>4</sub> (reaction (13)). These radicals are formed mainly at the surface of the catalyst, a reaction that is not included in the model.

A comparable model calculation was carried out with O<sub>2</sub> as the oxidant. In this variation, reaction (8) was replaced by



reaction (8') was replaced by



and  $k_{15}$  was adjusted to obtain the CH<sub>4</sub> conversion reported in Table 4. Good agreement was found with  $k_{15} = 2.20 \times 10^{12} e^{-27,000/T} \text{ s}^{-1}$ . At 680°C,  $k_{15}$  is approximately a factor of 14 greater than  $k_8$ . The calculated C<sub>2+</sub> selectivity with 30 kPa CH<sub>4</sub> and 5.6 kPa O<sub>2</sub> was 87% at 680°C, which is much greater than the experimentally observed value of

62%. This observation supports the hypothesis that O<sub>2</sub> reacts with the surface to form another type of active center which is particularly nonselective. At these temperatures and pressures gas phase reactions do not serve as a major pathway for the formation of CO<sub>2</sub>.

## CONCLUSIONS

Although N<sub>2</sub>O is an effective oxidant for the CH<sub>4</sub> coupling reaction, the rate of oxygen incorporation into the catalyst is slower than with O<sub>2</sub>, which means that even at relatively small CH<sub>4</sub>/N<sub>2</sub>O ratios the overall reaction is limited by this step. At a given level of conversion much greater C<sub>2+</sub> selectivities were observed with N<sub>2</sub>O than with O<sub>2</sub>. The increase in selectivity with N<sub>2</sub>O is attributed to a decrease in CO<sub>x</sub> forming reactions on the surface of the catalyst. The heterogeneous part of the mechanism is similar with N<sub>2</sub>O and O<sub>2</sub>; however, additional steps are required to account for the decomposition of N<sub>2</sub>O and the fact that CH<sub>4</sub> inhibits the rate of N<sub>2</sub>O decomposition. The poor selectivity observed with the MgO catalyst indicates that this pure oxide is intrinsically nonselective, independent of the oxidant.

## ACKNOWLEDGMENT

The authors acknowledge financial support of this research by the National Science Foundation under Grant CHE-9005808.

## REFERENCES

1. Otsuka, K., and Nakajima, T., *J. Chem. Soc. Faraday Trans. 1* **83**, 1315 (1987).
2. Hutchings, G. J., Scurrall, M. S., and Woodhouse, J. R., *J. Chem. Soc. Chem. Commun.*, 1388 (1987).
3. Hutchings, G. J., Scurrall, M. S., and Woodhouse, J. R., *J. Chem. Soc. Faraday Trans. 1* **85**, 2507 (1989).
4. Hutchings, G. J., and Scurrall, M. S., in "Methane Conversion by Oxidative Processes" (E. E. Wolf, Ed.), p. 200. Van Nostrand-Reinhold, New York, 1992.
5. Shi, C., Hatano, M., and Lunsford, J. H., *Catal. Today* **13**, 191 (1992).
6. Wong, N. B., and Lunsford, J. H., *J. Chem. Phys.* **56**, 2664 (1972).
7. Takita, Y., and Lunsford, J. H., *J. Phys. Chem.* **83**, 683 (1979).

8. Martir, W., and Lunsford, J. H., *J. Am. Chem. Soc.* **103**, 3728 (1981).
9. Dell, R. M., Stone, F. S., and Tiley, P. F., *Trans. Faraday Soc.* **49**, 201 (1953).
10. Winter, E. R. S., *J. Catal.* **15**, 144 (1969).
11. Roos, J. A., Korf, S. J., Veehof, R. H. J., Van Ommen, J. G., and Ross, J. R. H., *Appl. Catal.* **52**, 131 (1989).
12. Satterfield, C. N., "Heterogeneous Catalysis in Practice," 1st ed., p. 53. McGraw-Hill, New York, 1980.
13. Shi, C., Xu, M., Rosynek, M. P., and Lunsford, J. H., *J. Phys. Chem.* **97**, 216 (1993).
14. Lunsford, J. H., Lin, C.-H., Wang, J.-X., and Campbell, K. D., in "Microstructure and Properties of Catalysts" (M. M. J. Treacy, J. M. Thomas, and J. M. White, Eds.), p. 305. Materials Research Society, Pittsburgh, 1988.
15. Xu, M., Shi, C., Rosynek, M. P., and Lunsford, J. H., *J. Phys. Chem.* **96**, 6395 (1992).
16. Ito, T., Wang, J.-X., Lin, C.-H., and Lunsford, J. H., *J. Am. Chem. Soc.* **107**, 5062 (1985).
17. Iwamoto, M., and Lunsford, J. H., *Chem. Phys. Lett.* **66**, 48 (1979).
18. Westley, F., Herron, J. T., Cvetanovic, R. J., Hampson, R. F., and Mallard, G., NIST Chemical Kinetics Database, Version 3.0, National Institute of Standards and Technology, U.S. Department of Commerce, 1991.
19. Tsang, W., *J. Phys. Chem. Ref. Data.* **17**, 887 (1988).
20. Chappell, G. A., and Shaw, H., *J. Phys. Chem.* **72**, 4672 (1968).
21. Warnatz, J., in "Combustion Chemistry" (W. C. Gardiner, Ed.), p. 197. Springer-Verlag, New York, 1984.
22. Allara, D. L., and Shaw, R., *J. Phys. Chem. Ref. Data.* **9**, 523 (1980).
23. Gutman, D., Lutz, R. W., Jacobs, N. F., and Hardwidge, E. A., *J. Chem. Phys.* **48**, 5689 (1968).
24. Sugawara, K., Okazaki, K., and Sato, S., *Bull. Chem. Soc. Jpn.* **54**, 2872 (1981).